

FIG. 8.69

Substituting the open-circuit equivalent for the balance arm of a balanced bridge.

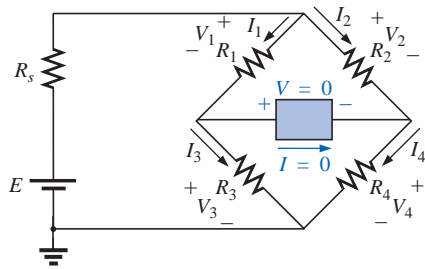


FIG. 8.70

Establishing the balance criteria for a bridge network.

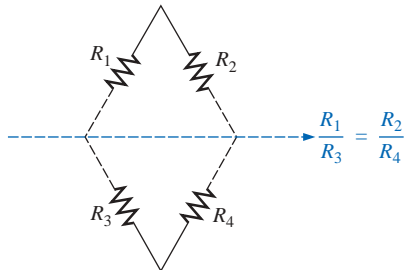


FIG. 8.71

A visual approach to remembering the balance condition.

and

$$I_1 R_1 = I_2 R_2$$

or

$$I_1 = \frac{I_2 R_2}{R_1}$$

In addition, when  $V = 0$  V,

$$V_3 = V_4$$

and

$$I_3 R_3 = I_4 R_4$$

If we set  $I = 0$  A, then  $I_3 = I_1$  and  $I_4 = I_2$ , with the result that the above equation becomes

$$I_1 R_3 = I_2 R_4$$

Substituting for  $I_1$  from above yields

$$\left(\frac{I_2 R_2}{R_1}\right) R_3 = I_2 R_4$$

or, rearranging, we have

$$\boxed{\frac{R_1}{R_3} = \frac{R_2}{R_4}} \tag{8.4}$$

This conclusion states that if the ratio of  $R_1$  to  $R_3$  is equal to that of  $R_2$  to  $R_4$ , the bridge will be balanced, and  $I = 0$  A or  $V = 0$  V. A method of memorizing this form is indicated in Fig. 8.71.

For the example above,  $R_1 = 4 \Omega$ ,  $R_2 = 2 \Omega$ ,  $R_3 = 2 \Omega$ ,  $R_4 = 1 \Omega$ , and

$$\frac{R_1}{R_3} = \frac{R_2}{R_4} \rightarrow \frac{4 \Omega}{2 \Omega} = \frac{2 \Omega}{1 \Omega} = 2$$

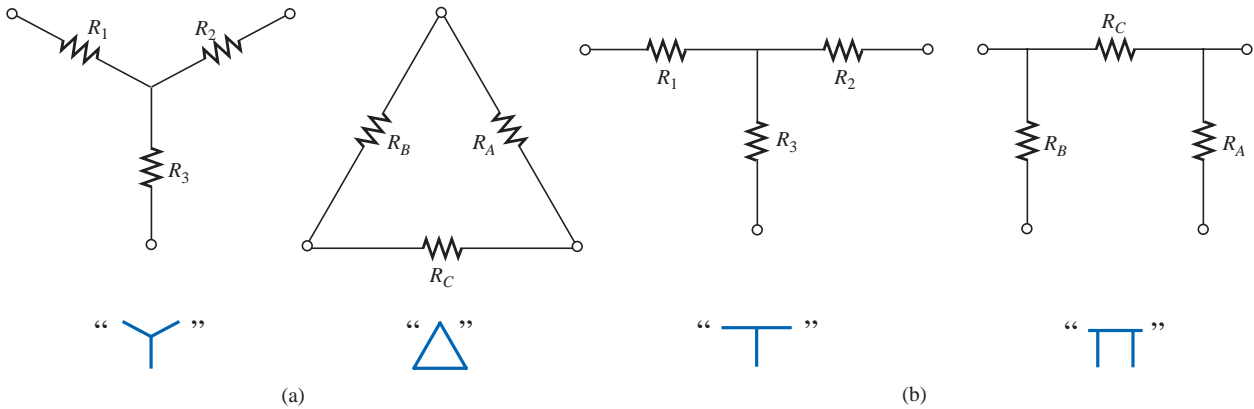
The emphasis in this section has been on the balanced situation. Understand that if the ratio is not satisfied, there will be a potential drop across the balance arm and a current through it. The methods just described (mesh and nodal analysis) will yield any and all potentials or currents desired, just as they did for the balanced situation.

### 8.12 Y-Δ (T-π) AND Δ-Y (π-T) CONVERSIONS

Circuit configurations are often encountered in which the resistors do not appear to be in series or parallel. Under these conditions, it may be necessary to convert the circuit from one form to another to solve for



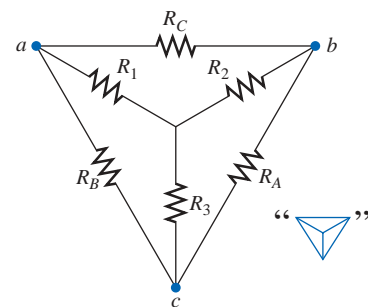
any unknown quantities if mesh or nodal analysis is not applied. Two circuit configurations that often account for these difficulties are the **wye (Y)** and **delta (Δ)** configurations, depicted in Fig. 8.72(a). They are also referred to as the **tee (T)** and **pi (π)**, respectively, as indicated in Fig. 8.72(b). Note that the pi is actually an inverted delta.



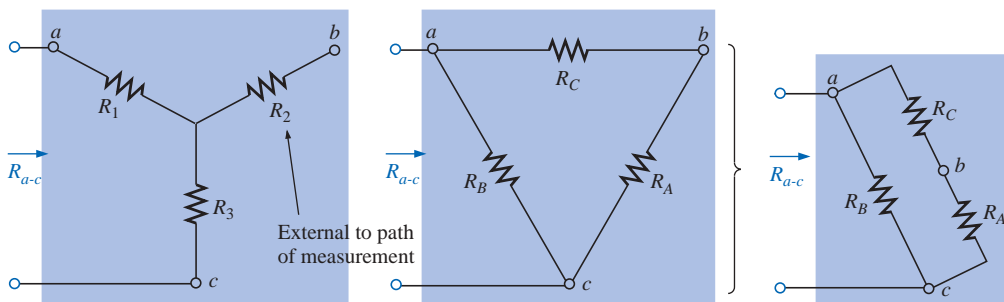
**FIG. 8.72**  
The Y (T) and Δ (π) configurations.

The purpose of this section is to develop the equations for converting from Δ to Y, or vice versa. This type of conversion will normally lead to a network that can be solved using techniques such as those described in Chapter 7. In other words, in Fig. 8.73, with terminals *a*, *b*, and *c* held fast, if the wye (Y) configuration were desired *instead of* the inverted delta (Δ) configuration, all that would be necessary is a direct application of the equations to be derived. The phrase *instead of* is emphasized to ensure that it is understood that only one of these configurations is to appear at one time between the indicated terminals.

It is our purpose (referring to Fig. 8.73) to find some expression for  $R_1$ ,  $R_2$ , and  $R_3$  in terms of  $R_A$ ,  $R_B$ , and  $R_C$ , and vice versa, that will ensure that the resistance between any two terminals of the Y configuration will be the same with the Δ configuration inserted in place of the Y configuration (and vice versa). If the two circuits are to be equivalent, the total resistance between any two terminals must be the same. Consider terminals *a-c* in the Δ-Y configurations of Fig. 8.74.



**FIG. 8.73**  
Introducing the concept of Δ-Y or Y-Δ conversions.



**FIG. 8.74**  
Finding the resistance  $R_{a-c}$  for the Y and Δ configurations.



Let us first assume that we want to convert the  $\Delta (R_A, R_B, R_C)$  to the Y  $(R_1, R_2, R_3)$ . This requires that we have a relationship for  $R_1, R_2$ , and  $R_3$  in terms of  $R_A, R_B$ , and  $R_C$ . If the resistance is to be the same between terminals  $a-c$  for both the  $\Delta$  and the Y, the following must be true:

$$R_{a-c} (Y) = R_{a-c} (\Delta)$$

so that 
$$R_{a-c} = R_1 + R_3 = \frac{R_B(R_A + R_C)}{R_B + (R_A + R_C)} \quad (8.5a)$$

Using the same approach for  $a-b$  and  $b-c$ , we obtain the following relationships:

$$R_{a-b} = R_1 + R_2 = \frac{R_C(R_A + R_B)}{R_C + (R_A + R_B)} \quad (8.5b)$$

and 
$$R_{b-c} = R_2 + R_3 = \frac{R_A(R_B + R_C)}{R_A + (R_B + R_C)} \quad (8.5c)$$

Subtracting Eq. (8.5a) from Eq. (8.5b), we have

$$(R_1 + R_2) - (R_1 + R_3) = \left( \frac{R_C R_B + R_C R_A}{R_A + R_B + R_C} \right) - \left( \frac{R_B R_A + R_B R_C}{R_A + R_B + R_C} \right)$$

so that 
$$R_2 - R_3 = \frac{R_A R_C - R_B R_A}{R_A + R_B + R_C} \quad (8.5d)$$

Subtracting Eq. (8.5d) from Eq. (8.5c) yields

$$(R_2 + R_3) - (R_2 - R_3) = \left( \frac{R_A R_B + R_A R_C}{R_A + R_B + R_C} \right) - \left( \frac{R_A R_C - R_B R_A}{R_A + R_B + R_C} \right)$$

so that 
$$2R_3 = \frac{2R_B R_A}{R_A + R_B + R_C}$$

resulting in the following expression for  $R_3$  in terms of  $R_A, R_B$ , and  $R_C$ :

$$R_3 = \frac{R_A R_B}{R_A + R_B + R_C} \quad (8.6a)$$

Following the same procedure for  $R_1$  and  $R_2$ , we have

$$R_1 = \frac{R_B R_C}{R_A + R_B + R_C} \quad (8.6b)$$

and 
$$R_2 = \frac{R_A R_C}{R_A + R_B + R_C} \quad (8.6c)$$

*Note that each resistor of the Y is equal to the product of the resistors in the two closest branches of the  $\Delta$  divided by the sum of the resistors in the  $\Delta$ .*



To obtain the relationships necessary to convert from a Y to a Δ, first divide Eq. (8.6a) by Eq. (8.6b):

$$\frac{R_3}{R_1} = \frac{(R_A R_B)/(R_A + R_B + R_C)}{(R_B R_C)/(R_A + R_B + R_C)} = \frac{R_A}{R_C}$$

or 
$$R_A = \frac{R_C R_3}{R_1}$$

Then divide Eq. (8.6a) by Eq. (8.6c):

$$\frac{R_3}{R_2} = \frac{(R_A R_B)/(R_A + R_B + R_C)}{(R_A R_C)/(R_A + R_B + R_C)} = \frac{R_B}{R_C}$$

or 
$$R_B = \frac{R_3 R_C}{R_2}$$

Substituting for  $R_A$  and  $R_B$  in Eq. (8.6c) yields

$$\begin{aligned} R_2 &= \frac{(R_C R_3/R_1)R_C}{(R_3 R_C/R_2) + (R_C R_3/R_1) + R_C} \\ &= \frac{(R_3/R_1)R_C}{(R_3/R_2) + (R_3/R_1) + 1} \end{aligned}$$

Placing these over a common denominator, we obtain

$$\begin{aligned} R_2 &= \frac{(R_3 R_C/R_1)}{(R_1 R_2 + R_1 R_3 + R_2 R_3)/(R_1 R_2)} \\ &= \frac{R_2 R_3 R_C}{R_1 R_2 + R_1 R_3 + R_2 R_3} \end{aligned}$$

and

$$R_C = \frac{R_1 R_2 + R_1 R_3 + R_2 R_3}{R_3} \tag{8.7a}$$

We follow the same procedure for  $R_B$  and  $R_A$ :

$$R_A = \frac{R_1 R_2 + R_1 R_3 + R_2 R_3}{R_1} \tag{8.7b}$$

and

$$R_B = \frac{R_1 R_2 + R_1 R_3 + R_2 R_3}{R_2} \tag{8.7c}$$

*Note that the value of each resistor of the Δ is equal to the sum of the possible product combinations of the resistances of the Y divided by the resistance of the Y farthest from the resistor to be determined.*

Let us consider what would occur if all the values of a Δ or Y were the same. If  $R_A = R_B = R_C$ , Equation (8.6a) would become (using  $R_A$  only) the following:

$$R_3 = \frac{R_A R_B}{R_A + R_B + R_C} = \frac{R_A R_A}{R_A + R_A + R_A} = \frac{R_A^2}{3R_A} = \frac{R_A}{3}$$

and, following the same procedure,

$$R_1 = \frac{R_A}{3} \quad R_2 = \frac{R_A}{3}$$



In general, therefore,

$$R_Y = \frac{R_\Delta}{3} \tag{8.8a}$$

or

$$R_\Delta = 3R_Y \tag{8.8b}$$

which indicates that for a Y of three equal resistors, the value of each resistor of the Δ is equal to three times the value of any resistor of the Y. If only two elements of a Y or a Δ are the same, the corresponding Δ or Y of each will also have two equal elements. The converting of equations will be left as an exercise for the reader.

The Y and the Δ will often appear as shown in Fig. 8.75. They are then referred to as a **tee (T)** and a **pi (π)** network, respectively. The equations used to convert from one form to the other are exactly the same as those developed for the Y and Δ transformation.

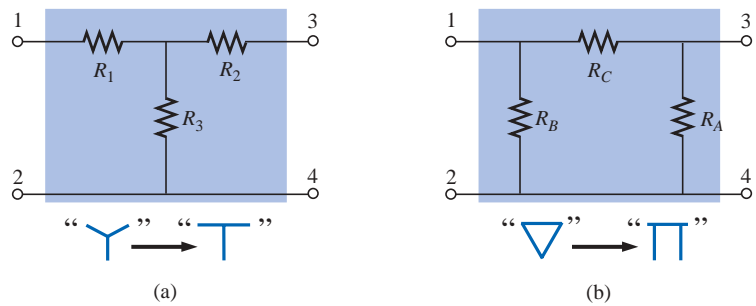


FIG. 8.75

The relationship between the Y and T configurations and the Δ and π configurations.

**EXAMPLE 8.27** Convert the Δ of Fig. 8.76 to a Y.

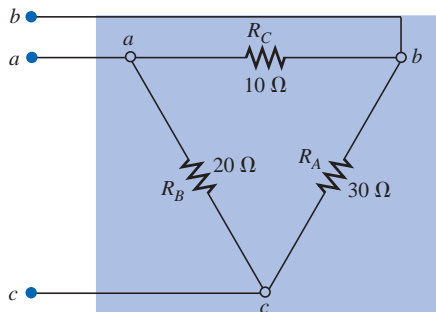


FIG. 8.76

Example 8.27.

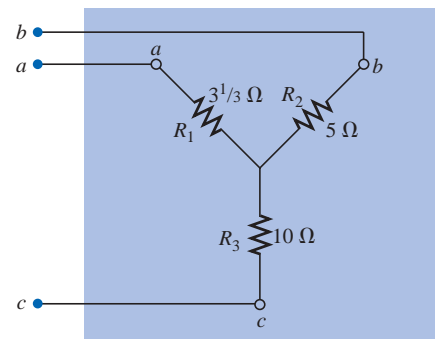


FIG. 8.77

The Y equivalent for the Δ of Fig. 8.76.



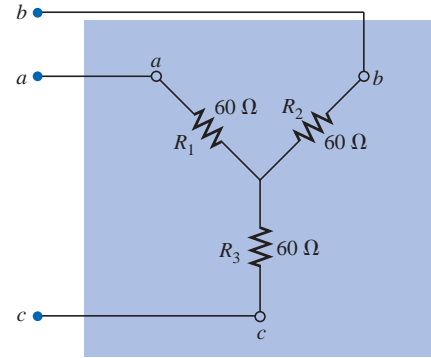
**Solution:**

$$R_1 = \frac{R_B R_C}{R_A + R_B + R_C} = \frac{(20 \Omega)(10 \Omega)}{30 \Omega + 20 \Omega + 10 \Omega} = \frac{200 \Omega}{60} = 3\frac{1}{3} \Omega$$

$$R_2 = \frac{R_A R_C}{R_A + R_B + R_C} = \frac{(30 \Omega)(10 \Omega)}{60 \Omega} = \frac{300 \Omega}{60} = 5 \Omega$$

$$R_3 = \frac{R_A R_B}{R_A + R_B + R_C} = \frac{(20 \Omega)(30 \Omega)}{60 \Omega} = \frac{600 \Omega}{60} = 10 \Omega$$

The equivalent network is shown in Fig. 8.77 (page 298).



**FIG. 8.78**  
Example 8.28.

**EXAMPLE 8.28** Convert the Y of Fig. 8.78 to a Δ.

**Solution:**

$$R_A = \frac{R_1 R_2 + R_1 R_3 + R_2 R_3}{R_1}$$

$$= \frac{(60 \Omega)(60 \Omega) + (60 \Omega)(60 \Omega) + (60 \Omega)(60 \Omega)}{60 \Omega}$$

$$= \frac{3600 \Omega + 3600 \Omega + 3600 \Omega}{60} = \frac{10,800 \Omega}{60}$$

$R_A = 180 \Omega$

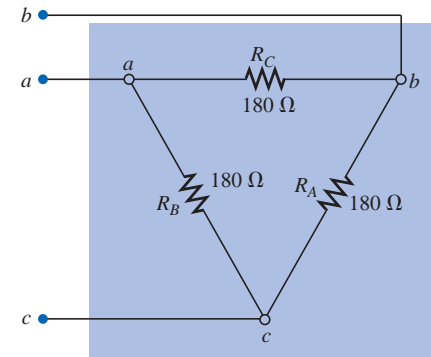
However, the three resistors for the Y are equal, permitting the use of Eq. (8.8) and yielding

$R_\Delta = 3R_Y = 3(60 \Omega) = 180 \Omega$

and

$R_B = R_C = 180 \Omega$

The equivalent network is shown in Fig. 8.79.



**FIG. 8.79**  
The Δ equivalent for the Y of Fig. 8.78.

**EXAMPLE 8.29** Find the total resistance of the network of Fig. 8.80, where  $R_A = 3 \Omega$ ,  $R_B = 3 \Omega$ , and  $R_C = 6 \Omega$ .

**Solution:**

Two resistors of the Δ were equal; therefore, two resistors of the Y will be equal.

$$R_1 = \frac{R_B R_C}{R_A + R_B + R_C} = \frac{(3 \Omega)(6 \Omega)}{3 \Omega + 3 \Omega + 6 \Omega} = \frac{18 \Omega}{12} = 1.5 \Omega$$

$$R_2 = \frac{R_A R_C}{R_A + R_B + R_C} = \frac{(3 \Omega)(6 \Omega)}{12 \Omega} = \frac{18 \Omega}{12} = 1.5 \Omega$$

$$R_3 = \frac{R_A R_B}{R_A + R_B + R_C} = \frac{(3 \Omega)(3 \Omega)}{12 \Omega} = \frac{9 \Omega}{12} = 0.75 \Omega$$

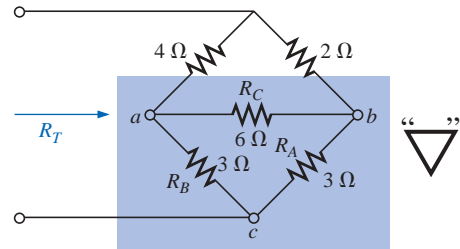
Replacing the Δ by the Y, as shown in Fig. 8.81, yields

$$R_T = 0.75 \Omega + \frac{(4 \Omega + 1.5 \Omega)(2 \Omega + 1.5 \Omega)}{(4 \Omega + 1.5 \Omega) + (2 \Omega + 1.5 \Omega)}$$

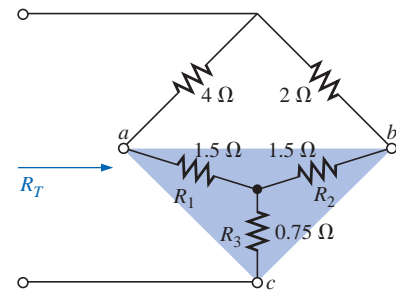
$$= 0.75 \Omega + \frac{(5.5 \Omega)(3.5 \Omega)}{5.5 \Omega + 3.5 \Omega}$$

$$= 0.75 \Omega + 2.139 \Omega$$

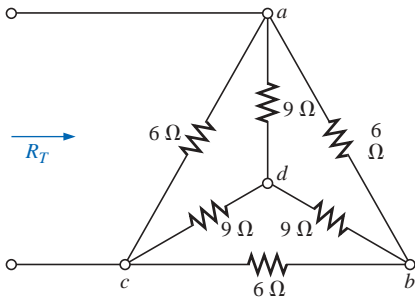
$R_T = 2.889 \Omega$



**FIG. 8.80**  
Example 8.29.



**FIG. 8.81**  
Substituting the Y equivalent for the bottom Δ of Fig. 8.80.



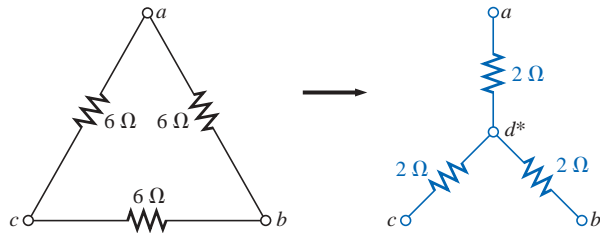
**FIG. 8.82**  
Example 8.30.

**EXAMPLE 8.30** Find the total resistance of the network of Fig. 8.82.

**Solutions:** Since all the resistors of the  $\Delta$  or Y are the same, Equations (8.8a) and (8.8b) can be used to convert either form to the other.

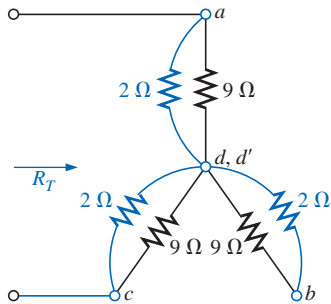
a. *Converting the  $\Delta$  to a Y.* Note: When this is done, the resulting  $d'$  of the new Y will be the same as the point  $d$  shown in the original figure, only because both systems are “balanced.” That is, the resistance in each branch of each system has the same value:

$$R_Y = \frac{R_\Delta}{3} = \frac{6\ \Omega}{3} = 2\ \Omega \quad (\text{Fig. 8.83})$$



**FIG. 8.83**

Converting the  $\Delta$  configuration of Fig. 8.82 to a Y configuration.



**FIG. 8.84**

Substituting the Y configuration for the converted  $\Delta$  into the network of Fig. 8.82.

The network then appears as shown in Fig. 8.84.

$$R_T = 2 \left[ \frac{(2\ \Omega)(9\ \Omega)}{2\ \Omega + 9\ \Omega} \right] = 3.2727\ \Omega$$

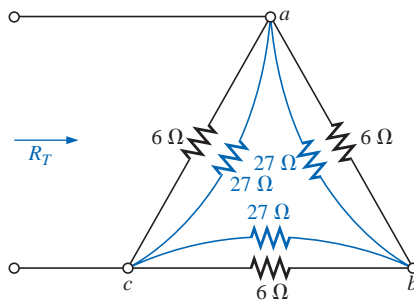
b. *Converting the Y to a  $\Delta$ :*

$$R_\Delta = 3R_Y = (3)(2\ \Omega) = 6\ \Omega \quad (\text{Fig. 8.85})$$

$$R'_T = \frac{(6\ \Omega)(27\ \Omega)}{6\ \Omega + 27\ \Omega} = \frac{162\ \Omega}{33} = 4.9091\ \Omega$$

$$R_T = \frac{R'_T(R'_T + R'_T)}{R'_T + (R'_T + R'_T)} = \frac{R'_T 2R'_T}{3R'_T} = \frac{2R'_T}{3} \\ = \frac{2(4.9091\ \Omega)}{3} = 3.2727\ \Omega$$

which checks with the previous solution.



**FIG. 8.85**

Substituting the converted Y configuration into the network of Fig. 8.82.