

Diode Rectifier Circuits

Basic Definition:

A diode circuit that converts an ac voltage to a pulsating dc voltage and permits current to flow in one direction only is called "*rectifier*" and the ac-to-dc conversion process is termed "*rectification*".

Half-Wave Rectifier (HWR):

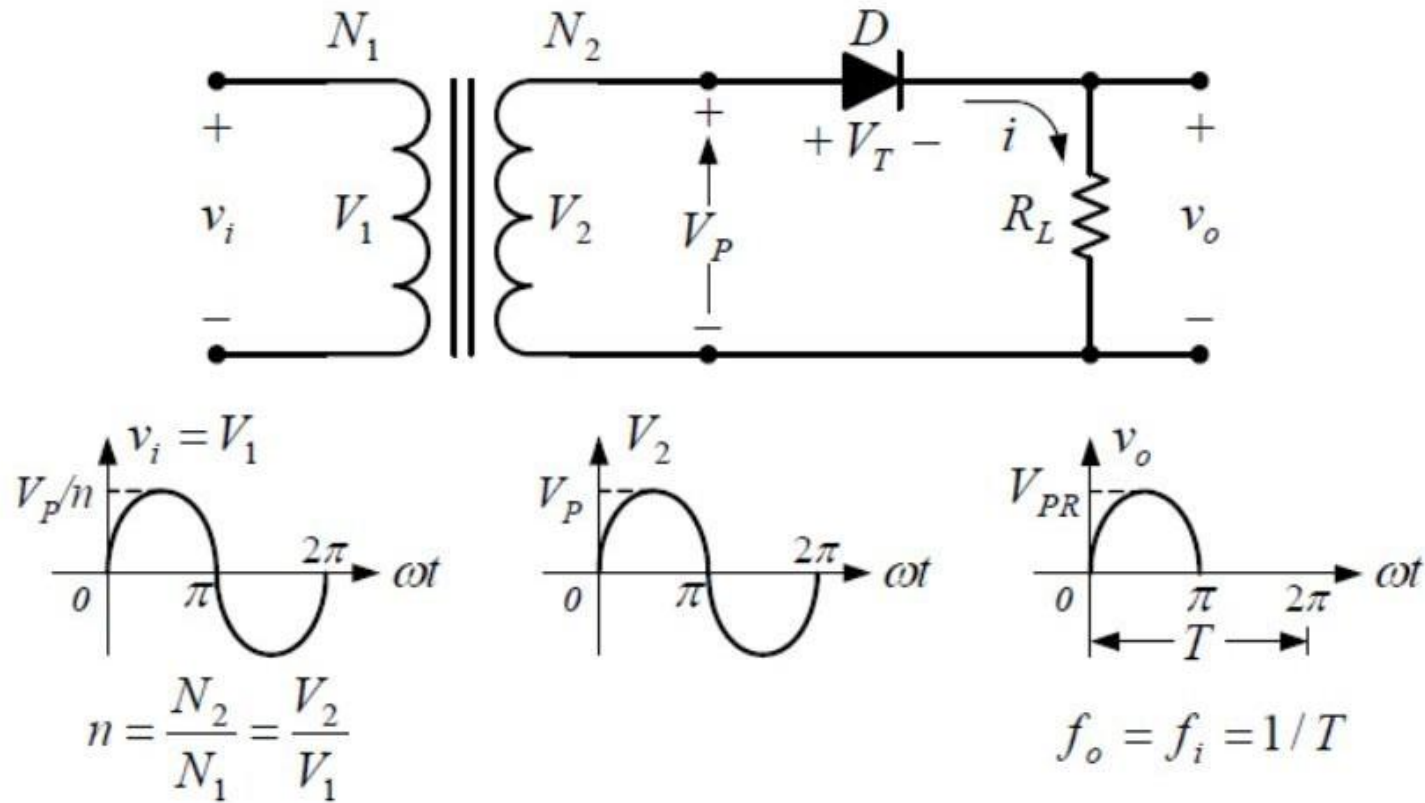


Fig. 5-1

For the half-wave rectifier circuit of Fig. 5-1:

◀ The average (dc) value of a half-wave rectified sine-wave voltage (V_{dc}) is

$$V_{dc} = \frac{1}{T} \int_0^T v_o(\omega t) \cdot d\omega t = \frac{1}{2\pi} \int_0^\pi V_{PR} \sin \omega t \cdot d\omega t = \frac{V_{PR}}{\pi}$$

For V_P close to V_T ,

$$\boxed{V_{dc} = 0.318(V_P - V_T)} \quad [5.1a]$$

For $V_P \gg V_T$,

$$\boxed{V_{dc} = 0.318V_P} \quad [5.1b]$$

◀ The root mean square (rms) value of the load voltage (V_{rms}) is

$$V_{rms} = \sqrt{\frac{1}{T} \int_0^T v_o^2(\omega t) \cdot d\omega t} = \sqrt{\frac{1}{2\pi} \int_0^\pi V_{PR}^2 \sin^2 \omega t \cdot d\omega t} = \frac{V_{PR}}{2}$$

For V_P close to V_T ,

$$\boxed{V_{rms} = 0.5(V_P - V_T)} \quad [5.2a]$$

For $V_P \gg V_T$,

$$\boxed{V_{rms} = 0.5V_P} \quad [5.2b]$$

- ◀ The rms value of the ac component (or *the ripple voltage*) of the rectified signal [$V_r(rms)$] is

$$V_r(rms) = \sqrt{V_{rms}^2 - V_{dc}^2} = \sqrt{(0.5V_{PR})^2 - (0.318V_{PR})^2} = 0.385V_{PR}$$

For V_P close to V_T ,

$$\boxed{V_r(rms) = 0.385(V_P - V_T)} \quad [5.3a]$$

For $V_P \gg V_T$,

$$\boxed{V_r(rms) = 0.385V_P} \quad [5.3b]$$

- ◀ The percent ripple (r) in the rectified waveform (also called *the ripple factor*) is

$$r = \frac{V_r(rms)}{V_{dc}} \times 100\% = \frac{0.385V_{PR}}{0.318V_{PR}} \times 100\% = 121\%$$

◀ Efficiency (η) = $[P_{dc}(load) / P_{total}(circuit)] \times 100\%$

$$\eta = \frac{I_{dc}^2 R_L}{I_{rms}^2 (r_d + R_L)} \times 100\% = \frac{(0.318I_P)^2 R_L}{(0.5I_P)^2 (r_d + R_L)} \times 100\% = \frac{40.5}{1 + r_d / R_L} \%$$

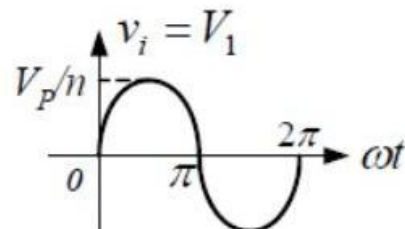
For ideal diode ($r_d = 0 \Omega$), $\eta = \eta_{max} = 40.5 \%$

◀ The peak inverse voltage (PIV) of the diode is

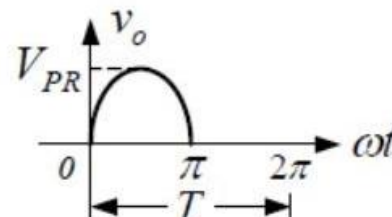
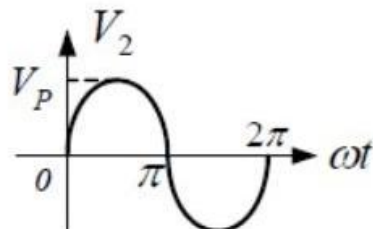
$$\boxed{PIV = V_P} \quad [5.4]$$

◀ The frequency of the output rectified signal (f_o) is

$$\boxed{f_o = f_i} \quad [5.5]$$



$$n = \frac{N_2}{N_1} = \frac{V_2}{V_1}$$



$$f_o = f_i = 1/T$$

Full-Wave Rectifiers (FWRs):

1. A Bridge Full-Wave Rectifier:

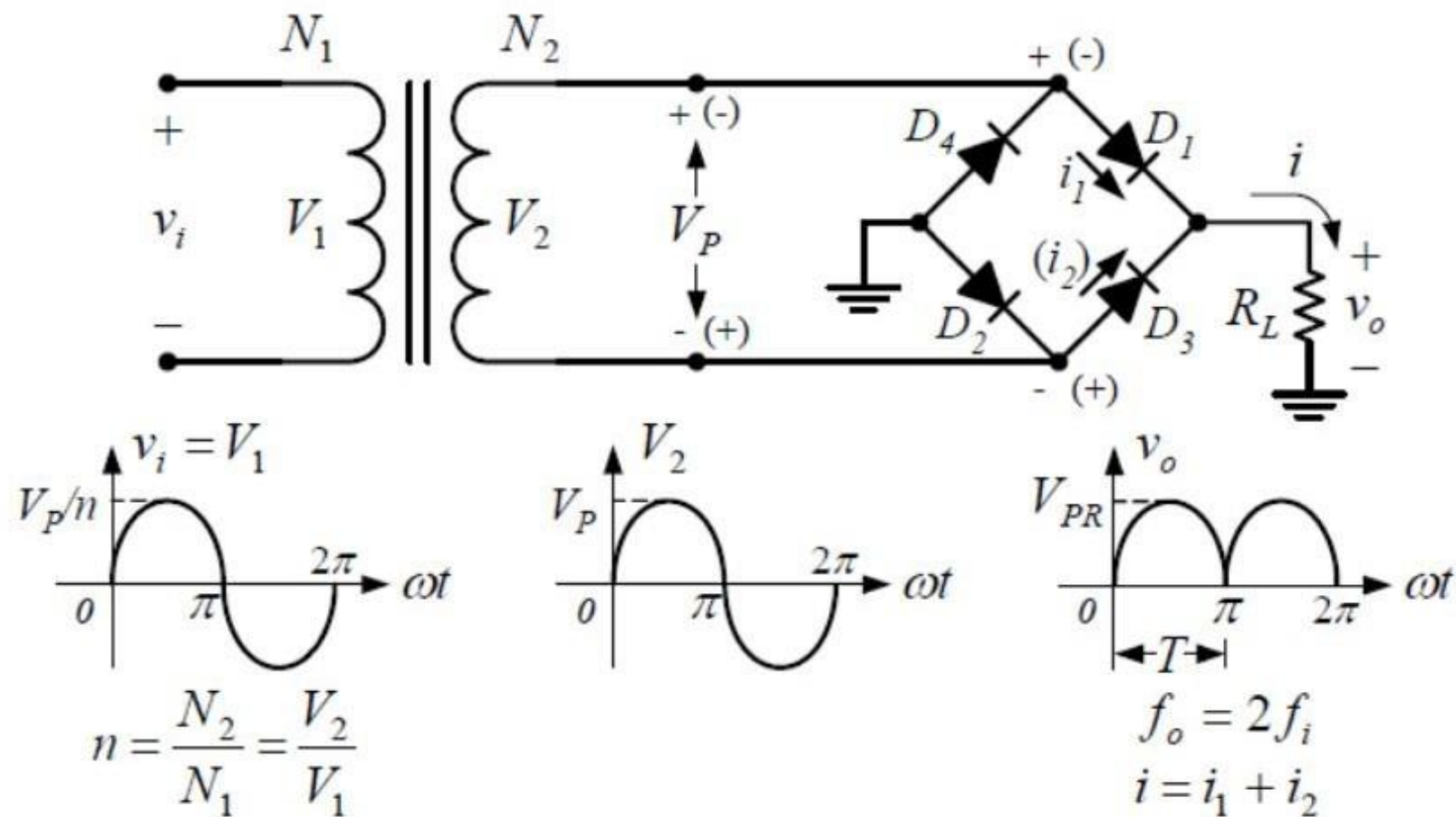


Fig. 5-2

For the bridge full-wave rectifier circuit of Fig. 5-2:

$$\blacktriangleleft V_{dc} = \frac{1}{\pi} \int_0^{\pi} V_{PR} \sin \omega t \cdot d\omega t = \frac{2V_{PR}}{\pi}$$

For V_P close to $2V_T$,

$$\boxed{V_{dc} = 0.636(V_P - 2V_T)} \quad [5.6a]$$

For $V_P \gg 2V_T$,

$$\boxed{V_{dc} = 0.636V_P} \quad [5.6b]$$

$$\blacktriangleleft V_{rms} = \sqrt{\frac{1}{\pi} \int_0^{\pi} V_{PR}^2 \sin^2 \omega t \cdot d\omega t} = \frac{V_{PR}}{\sqrt{2}}$$

For V_P close to $2V_T$,

$$\boxed{V_{rms} = 0.707(V_P - 2V_T)} \quad [5.7a]$$

For $V_P \gg 2V_T$,

$$\boxed{V_{rms} = 0.707V_P} \quad [5.7b]$$

$$\blacktriangleleft V_r(rms) = \sqrt{V_{rms}^2 - V_{dc}^2} = \sqrt{(0.707V_{PR})^2 - (0.636V_{PR})^2} = 0.308V_{PR}$$

For V_P close to $2V_T$,

$$\boxed{V_r(rms) = 0.308(V_P - 2V_T)} \quad [5.8a]$$

For $V_P \gg 2V_T$,

$$\boxed{V_r(rms) = 0.308V_P} \quad [5.8b]$$

$$\blacktriangleleft r = \frac{V_r(rms)}{V_{dc}} \times 100\% = \frac{0.308V_{PR}}{0.636V_{PR}} \times 100\% = 48.4\%$$

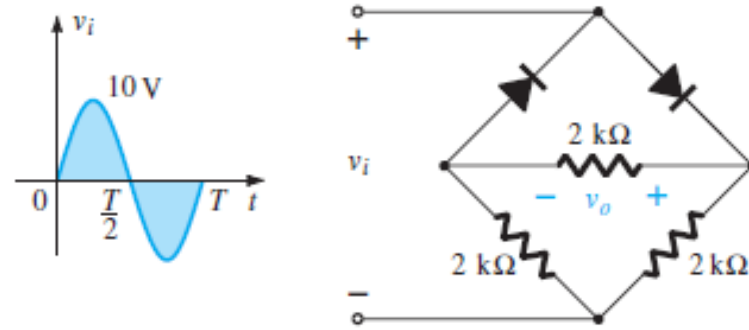
$$\blacktriangleleft \eta = \frac{I_{dc}^2 R_L}{I_{rms}^2 (2r_d + R_L)} \times 100\% = \frac{(0.636I_P)^2 R_L}{(0.707I_P)^2 (2r_d + R_L)} \times 100\% = \frac{81}{1 + 2r_d / R_L} \%$$

For ideal diode ($r_d = 0 \Omega$), $\eta = \eta_{max} = 81 \%$

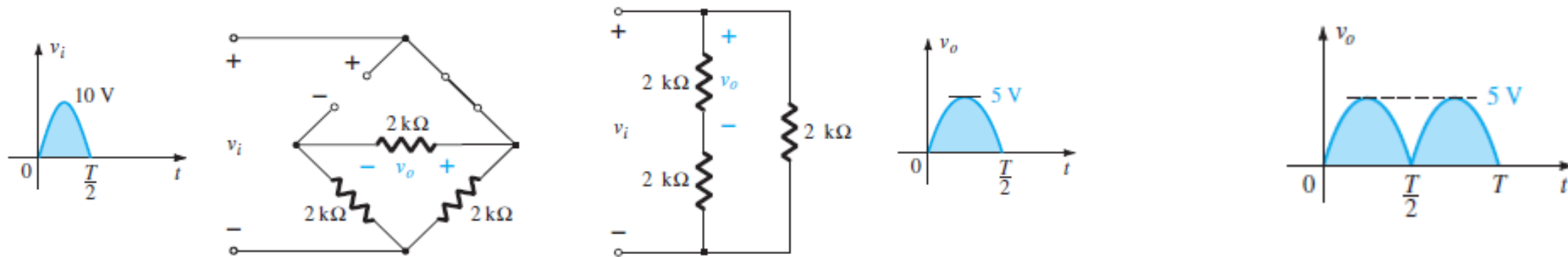
$$\blacktriangleleft \boxed{PIV = V_P - 2V_T} \quad [5.9]$$

$$\blacktriangleleft \boxed{f_o = 2f_i} \quad [5.10]$$

EXAMPLE : Determine the output waveform for the network of Figure below. Calculate the output dc level and the required PIV of each diode

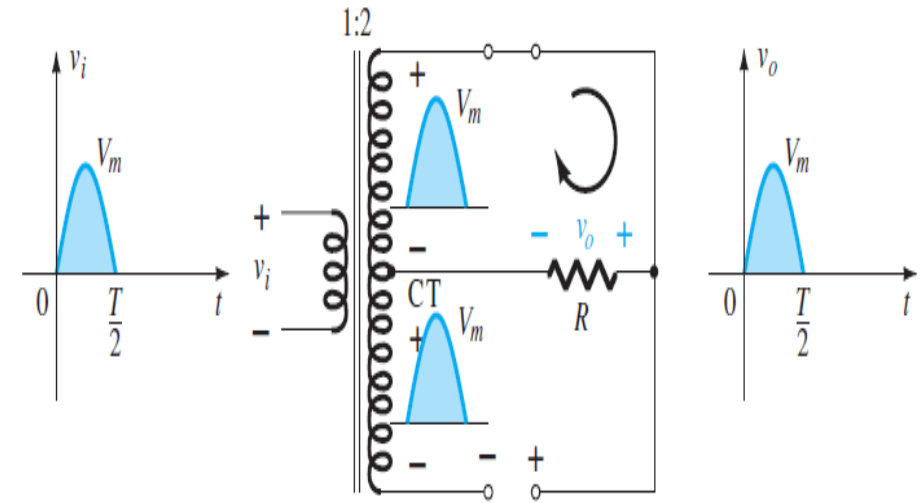
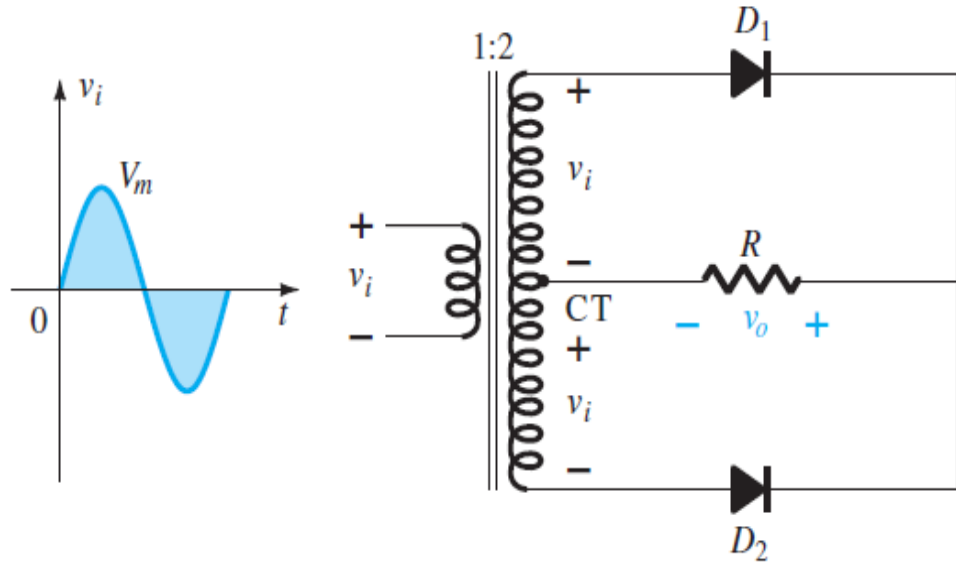


Solution: The network appears as shown in Fig.

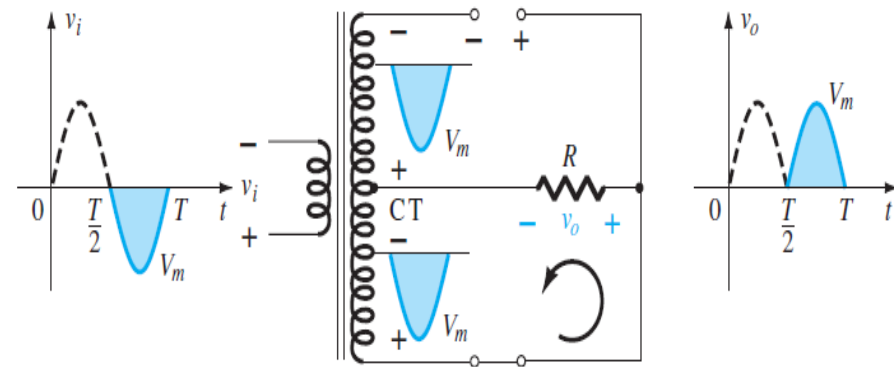


for the positive and negative region of the input voltage. Redrawing the network results in the configuration of Fig, where $v_o = 1/2(v_i)$, then $v_o = 1/2 (10 \text{ V}) = 5 \text{ V}$ and $V_{dc} = 0.636(5 \text{ V}) = 3.18 \text{ V}$.

2. A Center-Tapped (CT) Full-Wave Rectifier:



Center-tapped transformer full-wave rectifier.



For the center-tapped full-wave rectifier circuit

$$V_{dc} = 0.636(V_p - V_T)$$

$$V_{dc} = 0.636V_p$$

$$V_{rms} = 0.707(V_p - V_T)$$

$$V_{rms} = 0.707V_p$$

$$V_r(rms) = 0.308(V_p - V_T)$$

$$V_r(rms) = 0.308V_p$$

$$\begin{aligned} PIV &= V_{secondary} + V_R \\ &= V_m + V_m \end{aligned}$$

$$PIV = 2V_p - V_T$$

$$f_o = 2f_i$$

The average (dc) value

The root mean square (rms)

The (rms) value of the ripple voltage

